

DESIGN AND OPTIMIZATION OF MAGNETOSTRICTIVE STRAIN SENSOR

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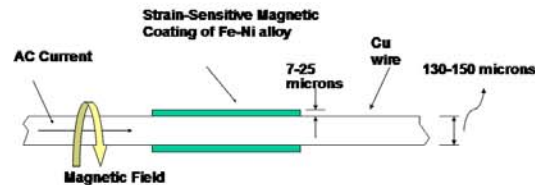
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OBJECTIVE

- Understand the mechanism and working of sensor
- Develop a model for magnetostrictive strain sensor
 - Indicate influence of all parameters sensor response
 - Study effect of stress/strain on sensor response
- Optimize sensor properties:
 - Range of strain
 - Sensitivity
 - Resolution
 - Repeatability

CONFIGURATION OF SENSOR

Configuration

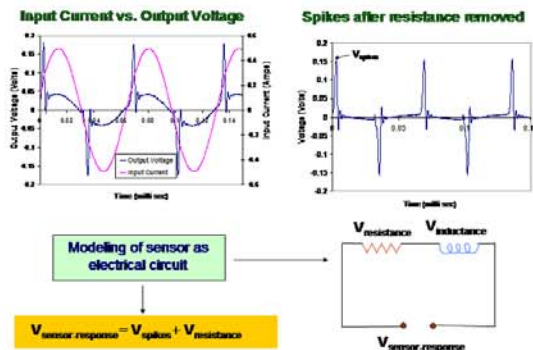


• Electrochemical deposition using Watt's nickel bath

MOTIVATION

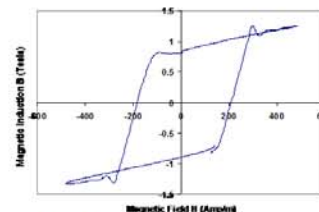
- Applications:
 - In service strain measurement
 - Cure information of resin
 - Health monitoring of structures
- Advantages:
 - Simple to examine response
 - Compared to Capacitance/Resistive Strain Gage
 - Better sensitivity; Less susceptible to noise
 - Higher dynamic range (>15KHz)
 - Compared to Fiber Optic Sensors
 - Lower cost - \$1 vs. \$50 per sensor; Easier to handle

SENSOR RESPONSE



ANALYSIS OF SENSOR RESPONSE

Occurrence of spikes → Hysteresis Loss



y-axis: $B = \frac{1}{A} \int V_{\text{inductance}} dt + \text{const.}$

x-axis: $H = \frac{\ln(1 + \frac{t_m}{r})}{2\pi t_m} I$

OPERATING PRINCIPLE

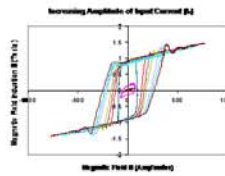
- Domain theory:
 - Application of strain → Change in permeability
 - Change in spike height ← Change in impedance
- Electromagnetic analysis:
 - $V_{\text{spikes}} = \frac{I}{2\pi} \ln\left(1 + \frac{t_m}{r}\right) \left[\mu_0 \cos \alpha t + \frac{\ln\left(1 + \frac{t_m}{r}\right)}{2\pi \mu_0} I_0^2 \sin \alpha t \cos \alpha t \frac{d\mu}{dt} \right]$
 - $\mu = \frac{M^2}{\lambda_0 \sigma + K_1} \frac{d\mu}{dt} = 0 \Rightarrow V_{\text{spikes}} = \frac{I}{2\pi} \ln\left(1 + \frac{t_m}{r}\right) \frac{M}{\sigma + H} I_0 \cos \alpha t$

Stress Analysis is

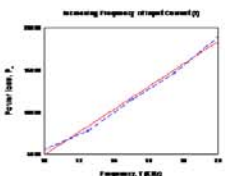
⁽¹⁾Cullity, B.D., *Introduction to Magnetic Materials*, Addison-Wesley Publishing Company, Inc., Reading, Mass. (1972).

RESULTS: PROOF OF MECHANISM

Amplitude: Saturation of curve



Frequency: Proof of Hysteresis



$$M = M_s \left(1 - \frac{a}{H} - \frac{b}{H^2} - \frac{c}{H^3} - \dots \right) + kT \quad [1]$$

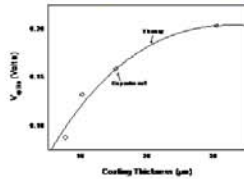
$$P = C_1 f + C_2 f^2 + C_3 f^3 \quad [2]$$

[1] Bozorth, R.M., *Ferromagnetism*, D. Van Nostrand Company, Inc., Toronto (1951).

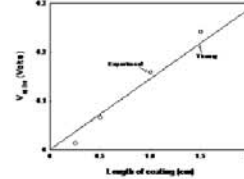
[2] Bertotti, G., *Hysteresis in Magnetism for Physicists, Materials Scientists, and Engineers*, Academic Press, Inc., San Diego (1998).

RESULTS: INFLUENCE OF MAGNETIC FILM

V_{spike} vs. Coating Thickness (t_m)



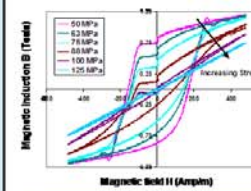
V_{spike} vs. Coating Length (l)



$$V_{spike} = -\frac{I}{2a} \ln \left(1 + \frac{t_m}{r} \right) + \mu_0 \mu_{rel} \cos \theta + \frac{\ln \left(1 + \frac{t_m}{r} \right)}{2a t_m} I_1^2 \sin \theta \cos \theta \frac{dt_m}{dt}$$

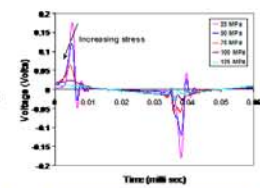
RESULTS: EFFECT OF STRESS

Effect of stress on hysteresis loop



B-H curve becomes more linear as stress increases

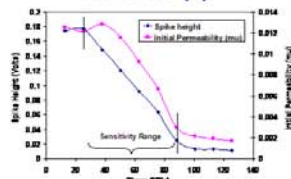
Effect of stress on spikes



Spike height decreases with increasing stress

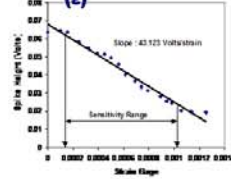
RESULTS: CALIBRATION OF SENSOR

V_{spike} and Permeability (μ) vs. Stress (σ)



Bare wire

V_{spike} and Strain (ϵ)



Embedded wire

Stress range (σ): 25-80 MPa

Strain range (ϵ): 0.01%-0.1%

CONCLUSIONS

- Occurrence of spikes due to hysteresis loss in magnetic coating
- Model accurately captures geometrical and process parameters
 - \uparrow in Stress/Strain \rightarrow \downarrow in V_{spike} \rightarrow within elastic limit of wire
 - \uparrow in length of coating \rightarrow linear \uparrow in V_{spike}
 - \uparrow in thickness of coating \rightarrow logarithmic \uparrow in V_{spike}
 - \uparrow in radius of copper wire \rightarrow \downarrow in V_{spike}
- Model can be used to tailor/optimize sensor
 - Range of strain: 0.01% - 0.1%
 - Sensitivity:
 - Resistive strain gage: ~ 2
 - Magnetostictive strain sensor: 1030

ACKNOWLEDGEMENTS

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